Friction losses in the pipe are much larger than the head available from the difference in elevations, therefore, pumping will be required. The most critical location in this regard is the section from Station 7 to Station 8 where approximately 4023 feet of head must be overcome. We have selected 3 positive displacement pumps (2 operating, 1 standby) each with an 800 hp motor and located at Station 1. It is possible that by locating smaller pumps -one at Station 2 and another at Station 6, the pump costs could be reduced. It should be noted, however, that any capital cost saving for the pumps could be offset by the cost of a power line to those locations. We did not make an economic study of this alternate.

6.2 WATER LINES - LAGUNA BRAVAS TO MINESITE AND MONTANDON

Based on previous studies done by MECA, Laguna Bravas appears to be the best source of water. Total water requirements amount to approximately 2000 gpm. Pumps will be required at Laguna Bravas (elev. 4215 meters) to provide water to the minesite (elev. 4515 meters), but once at the minesite, the portion needed to satisfy the mill at Montandon will flow by gravity.

The 450 hp pumps, one standby and the other two operating in series, will pump the water to the minesite. At that point approximately 1200 gpm will be diverted into a 1,500,000 gallon reservoir (tank) for distribution to points of need and the remainder, as required, will be piped to a 2,500,000 gallon reservoir (tank) at Montandon. The pipeline from the minesite to Montandon will be laid alongside the slurry line and on the same sleepers (see Figure 6-1).

Differences in head losses as well as flow quantities in various sections of the pipeline permitted changing the pipe sizes. In long pipelines such as this, considerable savings can be realized by optimizing pipe diameters. These changes are shown in the table below.

<u>Stations</u>	Length (ft)	Diam.(in)
L. Bravas -	3 75,460	12
3 - 4	46,010	10
4 - 9	134,950	8
9 - 10	52,500	6

It will be a welded joint steel pipe with a yield strength of 60,000 psi. We have included an allowance for 110 concrete anchors, 12 pressure relief valves and 12 blowoff valves.

6.3 TAILING LINE - MONTANDON TO TAILING DAM

According to the material balance, 1681 gpm of tailing will be generated in the tailing thickener at Montandon. For purposes of this study, we have selected a possible disposal area down the valley approximately 8 kilometers west of Montandon. Further investigation of this site must be done to determine suitability with respect to soil conditions and environmental impact. The area selected can impound 10 years accumulation of tailing with

impact. The area selected can impound 10 years accumulation of tailing with proper earth dam construction. We are, however, recommending a "starter" dam which can provide disposal for 3 years. The dam can be heightened in steps as required to reach full capacity.

The pipeline and pumps are sized for the ultimate dam height. Calculations are based on the pulp having a specific gravity of 1.38, the tailing thickener underflow pumps being located at elevation 2375 meters and top of dam being at 2275 meters.

Two pumps, one operating and one on standby, each with a 300 hp motor have been selected for this service. A 10" welded steel pipe will be used for the entire length. The pipe will be laid on sleepers set on a graded surface.

6.4 RECLAIM WATER LINE - TAILING DAM TO MONTANDON WATER RESERVOIR

Due to possible contaminations which could affect the process, we plan to reclaim only the cleanest portion of water from the tailing dam. Should later tests or operating conditions show that more water can be reclaimed, the amount of makeup water from Laguna Bravas can be reduced accordingly. Our pipeline and pumps at this time are based on reclaiming approximately 250 gpm. Two pumps, one operating and one standby, each with a 75 hp motor have been selected to pump this "clean" water back to the reservoir at Montandon. A 5" steel pipeline will be laid alongside the tailing line and utilize the same sleepers.



SECTION 7

FLOTATION AND REFINING AREA FACILITIES

This section covers the installations located in the vicinity of Montandon and includes both the process facilities and infrastructure. The area was chosen because of existing access by both road and rail, nearby availability of power and a comparatively level plantsite area considering the mountainous terrain. It is at an elevation of approximately 2400 meters. Drawing SK-02 (in Appendix) shows a conceptual plot plan of the area.

7.1 PROCESS DEVELOPMENT

The following paragraphs discuss the various aspects of process development in the beneficiation sections of the plant. The comminution evolution was described in Section 5.2. The work presented in this Section is based upon laboratory and other studies received by Parsons prior to September 1, 1988. A discussion of later laboratory work is contained in Section 12.

7.1.1 DESIGN BASIS

The flotation and refining section of the plant is designed to run concurrently with the grinding section. The design throughput is 360 dmtph. The methodology for arriving at that figure was discussed in detail in Section 5.2.1

7.1.2 PROCESS ASSUMPTIONS

The flowsheet consists of conventional sulfur flotation followed by thickening, filtration and drying of the concentrate prior to melting, sulfur filtration and sulfur forming. A certain amount of test work has been done on some samples of ore but this work cannot be considered sufficiently complete to allow for anything more than a conceptual approach to the development of a material balance and process flow diagram. The following paragraphs discuss the assumptions taken in the development of the process flow diagram:

A. The batch laboratory flotation results indicated that rougher and cleaner recoveries of approximately 87 and 93 percent, respectively, could be obtained from a feed sample assaying some 33 percent sulfur. Even though the actual anticipated feed assay is only 31.2 percent sulfur, considerably superior plant results should be obtainable based upon the indicated behavior of the samples and upon historical metallurgy elsewhere. Thus, Parsons has assumed the following results in the preparation of the material balance:

	Tonnes/	Assay	Recov.
	Hour	<u> </u>	Pct.
Rougher Flotation			
Feed	360	31.2	
Concentrate	180	60.68	97.25
First Cleaner Flotation			
Feed	185.57	60.64	
Concentrate	148.45	73.52	97
Second Cleaner Flotation			
Feed	148.45	73.52	
Concentrate	111.34	86.27	88
Cleaner Scavenger Flotation			
Feed	74.23	22.19	
Concentrate	5.57	59.18	20
Refinery			
Second Cleaner Concentrate	111.34	86.27	
Refined Sulfur	81.08	99.51	84
Overall Performance			
Feed	360	31.2	
Refined Sulfur	81.08	99.51	71.83

The recoveries in the first stages of flotation must be kept as high as possible, primarily because there is likely to be a fairly large loss of sulfur in the refining stage. During the melting stage, there will be a rejection of light (kuff) waste material and of coarse or heavy waste. This product may or may not be susceptible to flotation. Parsons, at this time has assumed that it cannot be satisfactorily retreated and the flowsheet shows it as being discarded. The alternative would be to regrind it and return it to the first cleaner flotation circuit. This would allow for a slower float in the rougher circuit and the corresponding production of less middlings by weight. The combined melter waste contains sulfur and it is this sulfur which is either lost or recovered as discussed above. In any event, it would be very expensive to return the melter sulfur-bearing waste product to the flotation circuit if that circuit were not adjacent to the refinery.

The flotation feed density has been maintained at 18 percent solids except in the scavenger where only 5.18 percent was possible. The flotation time in the rougher was dropped from the laboratory 5 minutes to 3 minutes (because of the lower feed assay), which was the time used for each phase of flotation. As is customary, the flotation cell capacity was augmented by the application of suitable factors which take into account cell volume occupied by machinery and air bubbles. These factors were 1.6, 1.5, 1.1 and 1.4 for the rougher, cleaner, recleaner and scavenger flotation banks, respectively.

- B. The thickeners were sized on the basis of from 0.3 to 0.4 square meters of area being required per tonne per day being fed to the machine. Flocculant is assumed to be needed in all cases, if not, thickener sizes would be larger than those selected.
- C. The disk filter used for dewatering the sulfur concentrate was sized on the basis of 400 kilograms of concentrate being recovered per square meter per hour.
- D. The Concentrate dryer was sized using an evaporation factor of 2.5. This is an experience factor which, when multiplied by the anticipated water removal in pounds/ hour, gives the dryer volume in cubic feet. A length to diameter ratio of 7.5:1 has been assumed for the dryer.
- E. Conditioners have been provided at both ends of the slurry pipe line, each being designed for one and a half hours of retention time and agitation.
- F. Process fresh water requirements appear to be less than seventy percent of the usual one tonne of water for each tonne of ore milled. However the water design is based on the standard of one-to-one. Thickeners have been provided at the grinding area and for both concentrate and tailing at the flotation area, which arrangement, together with the recovery of water from the tailing disposal area allows for zero discharge to the environment. There could be a greater recovery of water from the tailing pond since traditionally half of the water sent to the settling area can be recovered. However Parsons has chosen to recover somewhat less since there is a serious possibility of metallurgical problems if too much of the old water is reused. The test work has not taken into consideration the suitability of local water for metallurgical response and Parsons has had no choice but to assume, at this stage, that no undue problems will be encountered.
- It has been assumed that the contaminants in the dried flotation concentrate can be removed by melting. The melters have been designed as long rectangular vessels made of reinforced concrete equipped with heating coils, four mixers and suitable methods for decanting light waste and draining coarse or heavy waste. The addition of some 5 pounds of hydrated lime has been assumed as a satisfactory means for controlling the acidity of the sulfur fed to the leaf filters and also as a filter media. The pumps selected for handling "dirty molten sulfur" are, however, of a type which will not be adversely affected should diatomaceious earth have to be used as a filter media. The material balance around the melter/filter area is only of value as a guide since it shows more filter solids than would normally be permissible. The assumption has been made that the filter will be fed for a given length of time in closed circuit with the sulfur prior to commencing with the actual filtration. A complete cycle will take several hours after which a period of inactivity will be required before the filter can be opened for cleaning. While cleaning should be automatic according to the manufacturers, Parsons has allowed for personnel to aid in the performance of this duty. The wastes from the melter and from the sulfur filter all fall into a waste pit which will require periodic cleanup.

- H. The material in the waste pits will require digging and occasional drilling for removal. The product will be stockpiled for eventual covering with dirt prior to abandonment of the property. The environmental acceptability of such a procedure has not been investigated.
- I. Sulfur must be kept molten but not too hot. The viscosity of sulfur changes drastically at a temperature slightly over 300°F. Parsons has assumed that steam jacketing of pipes and valves handling molten sulfur will maintain the sulfur at a temperature not exceeding 280°F. Sulfur pumps will be supplied with steam at a pressure not to exceed 35 psig.
- J. No one form of sulfur forming has proven to be universally better than the others. Slates, water cooled prills, air cooled prills, pellets and granules are produced in various locations. However, slates, in terms of installed world-wide capacity, appear to be the most common method for forming sulfur. Parsons has for this reason and, also, because of cost, selected the slating method for this study. Other methods will provide a more satisfactory product from the point of view of dusting but the payment will probably not improve because of that fact. There is a possibility that slates might not be acceptable to some buyers so this should be determined during the next phase.
- K. The reader will note that quality control has been estimated as gross numbers under the heading of assaying, reagent preparation and instrumentation. These gross numbers need to be refined and distributed into their correct corresponding work areas during the feasibility study.
- L. Parsons has some concern over the quality of water available for use in sprays. For this reason we have selected dry dust collectors. However, in the generation of steam and in the sulfur forming process, we have had no alternative but to use water. (The smaller requirements for slating was another reason, albeit a minor one, for selecting that forming method over others). Possibly water can be reclaimed from the thickener overflows, but it may have to come from Lagunas Bravas or even from local wells.
- M. Some consideration has been given to treating the refinery tailing for additional recovery of sulfur values either alone or in combination with the original scavenger flotation concentrate*. While reportedly some success has been obtained in Chile when retreating refinery tailing, Parsons would be reluctant to include such treatment without specific test work on this ore. In any event, the refinery tailing will cool quickly and will have to be crushed and reground prior to any further flotation effort. If it is combined with scavenger concentrate, the regrinding can beneficially be done together. Because of the variable size of the refinery tailing, which may occur as fairly large slates or as lumps, an oversized jaw or roll crusher and a regrind mill, probably as large as 8 ft diameter by 12 ft long, will be required.

^{*}See Sections 5.1.2.I, 7.1.2.A and 12.5

7.1.3 MATERIAL BALANCES AND FLOWSHEETS

The material balances and corresponding flow diagrams are to be found in Section 5.1.3.

7.1.4 EQUIPMENT LIST

Table 7-1 shows the major equipment used in the beneficiation sections of the process facility. The same tabulation also shows unit horsepower, total connected horsepower and operating horsepower.

7.1.5 QUALITY CONTROL

The Mine Department will, from time to time, send samples to the quality control laboratory for analysis and evaluation. In addition to that, the process plant will need to constantly keep a check on grinding efficiency and plant behavior in general. The most important aspect of quality control is that the maximum amount of optimum grade sulfur is produced at the least possible cost. In order to accomplish this the metallurgist will sample the plant feed and tailing and the feed, concentrate and tailing from each individual circuit. The samples will be delivered to the laboratory for analysis and some samples will be evaluated by testing in the process laboratory to determine how to improve results. The following areas are required in the laboratory for the purposes shown:

	Square <u>Meters</u>
Routine Wet Analysis	30
Atomic Absorption	10
Balance Room	10
Ore Testing	35
Microscopy	5
Sample Preparation	
Dry Materials	30
Wet Sampling	30
Sulfur Samples	15
Toilets	15
Chemical Storage	40
Total Inside	220

Additionally some 30 cubic meters of space will be needed outside for such items as air compressors, vacuum pumps, venturi blowers and water demineralizers.

Equipment required will include such items as benches, hot plates, muffles, distilling apparatus, colorimeters, a flotation machine, pH meters, grinding and crushing apparatus, sieve shakers, magnetic separators, ovens, dust and fume handling apparatus, glassware and filtration equipment

Table 7-1 - Equipment List - Flotation and Refining

Key	Description	Size	Connected H P Each	H P	Operating H P
BA BB BC BD BE		48' dia x 56' 1 x 10 x 500 cu ft 1 x 8 x 300 cu ft 1 x 5 x 300 cu ft 1 x 7 x 500 cu ft 1 x 7 x 500 cu ft 125' x 10' SMD	125 400 240 150 280 7.5	125 400 240 150 280 7.5	125 404 240 150 280 7.5
B 6	Dryer Feed Conveyor Belt #P1	15 x 12' 6" disks 24" x 60', 300 fpm 12' x 85'	840 3 350	3	840 3 350
BI BJ BK	Dryer Discharge Conveyor Belt #P2 Radial Stacker Conveyor Belt #P3 Three Atmospheric Batch Sulfur Melters (each with 4 Mixers - 10' Shafts) Two Pre-Coated Steam-Jacketed Leaf Filters	24" x 20", 300 fpm 245" x 125", 300 fpm 25" x 125", 300 fpm 25" x 100"1 x 10"d	3 5 0 50	500	0.00
BM BN	Sulfur Storage Tank Sulfur Forming System Incl. 1 sulfur pit, 2 sulfur pumps, steam-jacketed pliping #/flow control & shut-off valves, 3 steam belt slaters	22 x 30	0	Ó	
BD BP BB BB	cooling system, piping, instr. & eng. Sulfur Stacking Conveyor Belt 4P4 Sulfur Load-Out Conveyor Belt 4P5 Articulated Front-Eng Loader	30° x 920°, 125 fpm 42° x 65°, 100 fpm 4.5 Cubic Yard Bucket 300006/Hr Boiler @ 55-60 psig (244 SPM Rupher [Funl)	150 30 20 0		150 30 20 0
BU BY BW	Steam Senerating System Four Flotation Multistage Air Blower Water Reservoir Tailing Thickener Four Clean-Up Vertical Pumps Air Compressor & 400 Gallon Receiver Sampling System Reagent Preparation & Distribution System	2500000 gallons 190' x 10' SWD 3' x 60" 637 ACFM 125 psi Allowance	7.5 20 150 3 20	3	7.5 26 150 20
54 68	6 Vertical Dirty Molten Sulfur Pumps 6 Vertical Dirty Molten Sulfur Pumps	4" x J-120" 4" x J-120"	15 15	90 90	30 30
62	2 Flotation Feed Slurry Pumps 2leaner Feed Slurry Pumps 2 ReCleaner Feed Slurry Pumps 2 ReCleaner Concentrate Slurry Pumps 2 Cleaner Scavenger Feed Slurry Pumps 2 Total Tailing Slurry Pumps 2 Concentrate Thickener Underflow Slurry Pumps 3 Tail. Thick. O'F Water Pumps (2 op 1 sp) 2 Pairs of Tail. Thick. U'F Pumps (2 op 2 sp) 2 Tailing Dam Reclaim Water Pumps Dn Barge	18" x 16" 14" x 12" 14" x 12" 10" x 10" 16" x 14" 22" x 20" 5 5" x 4" 10" x 12" x 14" Hor. (60' TDH) 6" x 6" 14 Stage 6"Bowl	150 100 75 50 125 250 15 125 250 75	100 250 500 30 375	100 75 50 125 250 15 250
36 38 41 43 46 50 62 63	Pump Box	10 cu m 5.2 cu m 4.2 cu m 3.1 cu m 7.7 cu m 16.9 cu m 2.1 cu m 14.7 cu m 2.1 cu m 1.0 cu m			
	Sub-Total Process Area			6739	4694
	Sub-Total Mine and Process Areas			19336.7	14921.7

7.2 MONTANDON PLANT INFRASTRUCTURE FACILITIES

In order to support the process operations at Montandon, the following facilities are required:

- Maintenance Shop and Warehouse
- Water Supply
- Power Supply
- Steam Generation
- Tailing Disposal
- Railroad
- Housing and Messhall Accommodations
 - Office and Laboratory

7.2.1 MAINTENANCE SHOP AND WAREHOUSE

These facilities will be housed in one structure about 15 meters wide and 46 meters long. The shop area will include a small machine shop, an electric shop, pipe and welding shop and a light vehicle repair shop. The warehouse will be large enough to store parts and material for both areas and include a large open fenced-in storage area for items which can be stored outside.

In addition to the above, there will be a fuelling station to dispense both diesel and gasoline fuel for the vehicles operating at the site.

7.2.2 WATER SUPPLY

A major source of process water will be obtained by reclaiming the water from the slurry piped from the grinding mill at the minesite. This water is reclaimed from the tailing thickener overflow, the concentrate thickener overflow and the tailing dam. Some makeup water will be obtained from the same source as the minesite supply. A separate pipeline alongside the slurry lines will be installed to transport this additional water requirement. All the reclaimed water and fresh water will be stored in a 2,500,000 gallon reservoir. The reservoir will be designed to maintain 100,000 gallons for fire protection. The reservoir will be located at an adequate elevation above the plantsite to provide the necessary pressure for all uses without pumping.

7.2.3 POWER SUPPLY

It has been assumed that adequate power from the national grid is available within a short distance from the plant. In our capital cost estimate we are including an allowance of a 10 kilometer transmission line from that source to the plantsite as well as a substation at the site.

7.2.4 STEAM GENERATION

Steam is required for the melters, leaf filters, liquid sulfur storage tank and all steam jacketed piping handling liquid sulfur. To provide

the necessary steam, a 30,000 lb/hr oil fired boiler is required. The unit supplies steam at 50-60 psig.

7.2.5 TAILING DISPOSAL

As noted in the flowsheet, Figure 5-2, the thickener underflow will be pumped and piped to a disposal area for settling the solids and reclaiming a portion of the water. With the maps available at this time it appears there is at least one suitable valley which can be "dammed" to provide an adequate disposal area within 10 kilometers of the plant site. Our capital cost estimate includes the cost of constructing an earth starter dam, a 10 kilometer pipeline to the dam and reclaim water pump and pipeline back to the plant water reservoir. Chile has rather stringent laws regarding location and design of tailing dams so these aspects must be carefully reviewed during the next phase of the project.

7.2.6 RAILROAD

Based on transporting the slurry from the mine to Montandon by pipeline, no new track will have to be constructed -except for a spur alongside the refined sulfur stockpile.

For the purposes of this study it is assumed that agreements can be reached with Codelco and the Government to use the existing railroads for shipping the refined sulfur to the port. This cost will be included in the operating cost estimate.

New or refurbished bottom dump rail cars will be required. For this study we are assuming the following:

- 40 metric tonne bottom dump cars
- 60,000 metric tons/month shipped from Montandon to Chanaral
- 146 kilometers from Montandon to Chanaral
- 3 day round trip (haul to Chanaral, dump cars, return to Montandon).
- 1 train load (2000 metric tons) each day of the month
 60,000 tonnes per month.

This would require 50 cars per day times 3 days per round trip or 150 cars. We are assuming locomotives to haul train are supplied by contract hauler in their haul price.



SECTION 8

PORT FACILITIES

Based on the investigations made by MECA and discussed in Chapter 3 of their report, Chanaral has been selected as the port providing the best facilities. Codelco, the present owners of the site and the related material handling and shiploading equipment, have constructed new port facilities leaving these older one idle. Renovation work will have to be done in the area to accommodate MECA's requirements, but by utilizing these facilities, capital costs will be minimized.

8.1 RAILCAR UNLOADING AND SULFUR STORAGE

The existing facilities include a railroad siding which passes over a dump hopper to receive the sulfur from bottom dump rail cars. The hopper feeds the material onto a 36" conveying system consisting of 3 belt conveyors in series, the last of which feeds the fixed stacking conveyor which in turn discharges the sulfur onto the storage yard. Renovation will consist of the following:

- o Removal of all existing conveyor components and replace with new -this includes idlers, pulleys, belts and motors.
- o Replacement of all electrical wiring.
- o Replacement of walkways alongside conveyors.
- Sandblasting and painting of conveyor support steel.
- o Cleanup, grading and bituminous surfacing of the storage yard.

8.2 SULFUR RECLAIM AND SHIP LOADING

The reclaim system under the storage yard is reported to be in good operational condition, so no renovation is necessary.

The existing ventilation system in the reclaim vault, however, is unsatisfactory and needs to be replaced. It is planned to install two exhaust fans, one at the end of each tunnel to pull the air from conveyor portal through the tunnels to obtain four air changes per hour.

The ship loader is reported to be in satisfactory operating conditions and requires no refurbishing.



SECTION 9

CAPITAL COST ESTIMATE

This section includes the basis for the capital cost estimate, a description of the various areas used in the breakdown of the estimate, the capital cost project summary and area cost work sheets. All data in this section is for base case only. See Section 13 for alternate case.

9.1 BASIS OF ESTIMATE

The following criteria itemizes the bases used in developing the estimate.

- o The estimate is "pre-feasibility" type and is a factored estimate based on RMP's historical data. The factor includes labor/material to install, hookup and support equipment.
- o Items <u>not</u> in factor include the following: (+/- 25% has been added to direct cost items for freight, OH & P)
 - Buildings
 - Roads/Railroads
 - Site Prep
 - Special Pipelines
 - Other Civil Work (Trailings Dam & Yard Cleanup)
 - Elect. Transmission or Generation
 - Power "to" Connect Point
- Chilean labor is based on \$5.00/Hr. all-in.
- o The "Factor" is pro-rated 70% for material and 30% for labor and indirects and OH & P.
- Equipment prices are budget quotations from reputable vendors.
- Costs of tanks, bins, boxes, etc. are based on steel tonnages calculated from preliminary sketches.
- o All costs are in 1988 U.S. Dollars.
- o No allowance for the following items is included:
 - Customs, duties or other tax
 - Overtime or other premium pay
 - Labor productivity
 - Equipment availability

9.2 PROJECT AREAS

The project has been divided into the following areas and the estimate is formatted in accordance with these areas.

Area	Description
5	Mine
10	From stockpile through ball mill feed conveyor
15	From ball mill to pipeline feed box and pumps
20	Slurry pipeline including feed box and pumps and pipeline discharge condition
30	From discharge conditioner through flotation, thickening, disk filter, dryer and melter feed
	conveyor.
40	Water supply system from Lagunas Bravas to and including the minesite and
	Montandon reservoirs
45	Tailing disposal including thickener, pipeline, dam and reclaim water system
.50	Power supply at minesite and Montandon
60	Auxiliary facilities, i.e., camp, shops, warehouse, office, laboratory, etc.
70	Port

9.3 ESTIMATE SUMMARY AND AREA WORK SHEETS

Table 9-1 shows the summary of the capital costs for the entire project. That table is followed by work sheets used to derive the costs for each of the areas described above.

|--|

Summary	
Estimate	
Cost	(000
Capital C	3/
9-1	
Table	

2	Description	Hejor Equip	NVE Sub Contract	Bulk Haterial	Labor & Indirect	Buildings	Roads & Railroad	Site Prep.	Pipeline & Sleepers	Other Civil	Special Elect.	lotal
S	Hine	4540					1010					2550
10	Crushing and Conveying	4612	1820	28651	2507	056		370			Q	16150
15	Grinding	2017	Ř	2064	985	336		344			8	0265
8	Slurry Pipeline	2731	138	4012	1720			8	7260			15938
8	Flotation, Filtration and Drying	3696	ĸ	3893	1669	480		230			110	10715
X	Nelting and Foreing	1689	356	7614	3263	710	1420	290			8	20880
9	Hater Supply	118	8 2	1821	553			8	8670		10	11490
45	Tailing and Reclaim Mater	485	116	673	582			460	1400	1250	01	4680
8	Power Supply	108	8	115	49	460		2			08%	10690
8	Auxiliary Facilities	151	33	88	*	3190		230			8	4090
2	Part	348		161	211	10	400			10		1470
	Sub Total	25902	3645	26092	11184	96136	2830	3224	17330	1260	0566	107553
	Home Office Engineering											10000
	Sub Total											117553
	Contingency (152)											17633
	TOTAL											135186

PAHSONS ESTIMATE WORKSHEET

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15 0. 350° 2424 6° 17 .75 Teccia: 15 - 0. 350° 2424 6° 16 . C Teccia: 10 - 40 (20) 6 . C 11 - 17 (20) 6 . C 12 (20) 6 . C 12 (20) 6 . C 12 (20) 6 . C 13 (20) 6 . C 14 (20) 6 . C 15 (20) 6 .	0.35° WALL	-	-							
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## 18/200 GF 9 .55 1607 1000 5000 100							-			
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if Values 10" & Aug 10 cA 400 20 Allow, Shali, Revis Revis (107 4000 1900 1900 1900 1900 1900 1900 1900	Fr Fisher was Printo	1		Sow			-			
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it Values 10"d Any 10 cf 400 20 Allow, Sharts, Revis Revisch (207 days 1900) (102 misc) 20 (207 days 1900) 21.1 20" & dy gg (40) 4139 500										
Allow, Shale, Revis, Revis, Revis, Aug 10 - 400 20 (10% mil.) (10%	Values			CZ			+			
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19:57	PRICED BY					DATE ///	200	-		SHEET		
JOB NO.: 6705-/ CLIE	CLIENT: MECA			TYPE OF ESTIMATE	TIMATE	PRE F	PEF FEASIBILITY.	- KUM		CHECKED BY	m)	R
DESCRIPTION CHILEDAN SULDWING STUDY	Sting STUDY	OUAN.	TIN	COST OR M/HRS	A/HRS	MATERIAL	8080	BUBCONTRACT		LABOR	T07/L	ار ا
LAZO STE PRED.				MATL M/H	M/H LABS		M/HR8	DOLLARS	M/HR8	DOLLARS		¥ L
For	de	02491	2	00/1				W Jy				111
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CER. JOHN O 14/811			+								0	0000

PAHSONS ESTIMATE WORKSHEET

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M.T.O. BY	7,000				0	1/88				SHEET		6
JOB NO.:	27/25-1		F	TYPE OF ESTIMATE	ATE PRE	_ ~	FEASIBILITY.		٥	снескер ву	1	ne
DESCRIPTIO	NO	- QUAN.	TIN	COST OR M/HRS	MATERIAL		SUBCONTRACT	L MT	Š	LABOR	- 2	TOT/L
ACCITY 4920	BUILDINGS			MATL M/H LABS		M/HR8	S DOLLARS		M/HRS	DOLLARS	+	
	FLOTATION FILTER	339000	4	180			278	28				
	506-100K13Ch12/2010%	275	6 6	30								\Box
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			H						111			
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	וחלטרי בשמנע	13500	3 4	7,79			1864	700			1	000
										2	0/51	3
			+									100000
CES:2000	CES.2000 0 (4/81)		H	H					H	H	H	

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PAHSONS ESTIMATE WORKSHEET

ASSACIATION & DEPLINA TITY SET STRANG ANTERNAL BUSCONTRACT LANGE ANTERNAL SUCCONTRACT LANGE ANTERNAL LANGE AND	M.T.O. BY				DAT	1///	88			SHEET	40
STATE AND STATE OF THE STATE OF	ON BO	6905-1 CLIENT: MECA		TYPE	OF ESTIMATE	Doc 6	18180	12.		CHECKED BY	Jul.
MATI, MIH LABS EACHOR MIHRS DOLLANS MANRES	JNIT/AF	TION CHILEDAY SUL CHUR STUDY			FR UNIT	MATERIAL	SUBCC	MTRACT	2	LABOR	
4-7 4-8 4-7 4-8 4-7 4-8 4-7 4-8 4-8 4-7 4-8 4-8 4-8 4-8 4-8 4-8 4-8 4-8 4-8 4-8	CCNT	Site Page					M/HR8	DOLLARS	14/14/18	DOLLARS	
Tayou Meer 30 1/260 8		May Favoal -			\frac{1}{2}						
	300	deco	8 00/1/					42000			
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FARSONS
ESTIMATE WORKSHEET

Stand Subcontract Mines Dolllars Mines Dolllars Mines Stands Stan					DAIE						
SCOUTH S STATE CLAKY STATE COST OF WITH STATE	COPOS-/ CLIENT:		TYPE	OF ESTIMATE		0077			CHECKED BY	(ma)	
ELECTRUM.	NGEN 30	OUAN.		F OR M/HRS		SUBCONTR	IACT	3	LABOR		اير
10. Seme 15.00		_				_	LLARS	M/HR8	DOLLARS		g
88, 81, 84, 81, 84, 81, 84, 81, 84, 81, 84, 81, 84, 81, 81, 81, 81, 81, 81, 81, 81, 81, 81	PAD MID. ONTRONE TYPE		2					960			
**************************************	LSEOKYA - SAME		2		2.8; dec			150			
	Total			38	8180			350	1280	00	
							-		80	22	9
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FAM-SONS ESTIMATE WORKSHEET

M.1.0. BY		100		_	DATE ///	88			SHEET		10
JOB NO.:	2925-		TYPE OF ESTIMATE	TIMATE	PRE FO	EASIGILITY	177.		CHECKED BY	1	1
UNIT/AREA DESCRIPTIO	ON CHILEGAL SULCHUR	OUAN.	COST OR M/HRS	A/HRS	MATERIAL	SUBCC	SUBCONTRACT	_	LABOR	F	TOTAL
CAPACITY		-	MATL	M/H LABS	CATCHOC	M/HR8	DOLLARS	MA/HPIB	DOLLARS		LU RE
ACCNI	SUMMARY										
0800	PACKAGED PLANTO				4 250 000		+			1	+
000	# STSIOH				9					I	1
400	EVRNACE C. FIRED HEATERS				312 000		912 000	6			<u> </u>
200	PUMPS & DRIVER				151 000						1
1600	7				200 000						-
1900	STORAGE TANKS	NO 17 17 17			1		144 680	6			1
2000					562 000						1
2200	SEPARATION EQUIPMENT				550 000						1
3700	MOBILE MINING COUIPMENT				195 000						$\frac{1}{1}$
1	•									1	+
											+
	SUB TOTAL				6 386 000		354000			I	t
	1										
-	TARISH	0/.8			211 000					1	+
	TOTAL MAJOR ENUPAINT				6 897000		3CL 600		1	I	t
							5	2.5			
	FACTORED POTAL.									91	087
1	Colorest					2	Brown	a			1
	Charles Designation		1				70000	2			1
	Sire Doe o						1000000	9 -			+
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	aran a			I			1			1	+
	6				-					1	+
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	ELEGT 30K				-					-	+
	TOTAL				The state of the s						1

PAMSONS
ESTIMATE WORKSHEET

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M.T.O. BY					DATE ///	88			SHEET	OF	
ON BOC	5805-1		TYP	TYPE OF ESTIMATE	Por	CEASIBILITY	.77		CHECKED BY	Drive.	1
UNIT/AREA DESCRIPTION	35 REPINING & FOR	OUAN.	7 IN	COST OR M/HRS	MATERIA	SUBCC	SUBCONTRACT	2	LABOR	TOTAL	
ACCITY	,		MATL	TL M/H LABS	_	M/HR8	DOLLARS	M/HRS	DOLLARS	MCD.	
assi	SLATING SYSTEM	353700	و	(0)			3 person				
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	A STOX.47		H 26H	36.							
	Tord!	1 11 1	\mathbb{H}								
		222/00	4				200			3	8
	STEAM GEN BLOG	371090	18	196			38				
	506- PX33X69X70110%	19:	91	100							
	GAR Dan Brook, Pax yes Blac To		0	300			Z46 000				
	INT FINISH - HOD		+				(000				
	Torac	37100	4				ADC DOD			lac	200
dep	Tapal Seed 36	370600	SF	(177)			(M. DOP			(Person)	18
			+						275	0 145	3
8.2000	CF8.2000 0 (4/81)		-							1016	4

FIAMSONS ESTIMATE WORKSHEET

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7 4/3200 Sy 1.00 E0		
1.00 ER		
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4800 Torge AREA 70		
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FAMSONS ESTIMATE WORKSHEET

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JOB NO.: 6925-1 CLIENT: MECA		TYPE	TYPE OF ESTIMATE	MATE	LOE	-E051	EDSIGIFIES	ار		CHECKEUBY	1	T
A 2 REPINING	OUAN.	116	COST OR M/HRS	70	MATERIAL		SUBCONTRACT	ACT	_	LABOR	TOT/ L	
APACITY		MATL	M/H LABS	_	EXFENSE	M/HR8	8 00	DOLLARS	SA/HERS	DOLLARS		-
BESC SITE PREP												
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FARSONS ESTIMATE WORKSHEET

JOB NO.: (CRESS-) CLIENT: CHILLE UNITIAREA AREA 35 REPUBLING FREMING DESCRIPTION CAPACITY ACCIT		TYP	TYPE OF ESTIMATE	-			١	
GREA 35 REPUBLIES	-		COL ESTIMATE			CHECKED BY	7	uni
	DUAN.	TIN	COST OR M/HRS PER UNIT	MATERIAL	SUBCONTRACT	LABOR		TOTAL
		O MATL	L M/H LABS	CALCASE	M/HRS DOLLARS	M/HRS DOLLARS		DOLLARS
FOR INTO DECIDENT THE		15		13000		100		
112.5XYA- 94871E		<i>B</i> 3		ag.		8		
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PAHSONS
ESTIMATE WORKSHEET

M.T.O. BY			100		_	DATE ///	8					SHEE .	•	40
JOB NO.:	6905-1		TYP	TYPE OF ESTIMATE	IMATE	PRE	FEBSIBILITY	11111	;		CHECK	CHECKED BY	1000	1
UNIT/AREA DESCRIPTION	ON CHILEON SULCHUR	GUAN.	8	COST OR M/HRS PER UNIT	/HRS	MATERIAL		BUBCONTRACT	MCT		LABOR		10	TOTAL
ACONT	Summag		MATT	H/M	M/H [AB\$		M/HRS	\vdash	DOLLANS	BA/Yeng	DOLLARS	LARS	8	5 I
1200	PUMPS & DRIVERS		+			100	S	H	\parallel			H	1	++
0061	1		H					Ш	200	Ш	\Box	H		111
	SUB TOTAL					000 601		Π	1 2					11:1
	FREIGHT	8.0	+			000 6	Q		H			H		
	TOTAL MATOR ENVIPMENT		-			811			88	0		Ш	#	
	CLECT CLECT CONC. SLETDER/AMMEN									111		H	7	77.0000
	SITE PREP							9	3 6	Ш			278	1 8
	TOTAL CANSTRE CAST WEEN 40		\mathbb{H}				Ш	Ш		Ш			1	18
	May Lacto													+++
	S. Cenpores 6.6		\mathbf{H}											
	Tapes 11490X		+										111	+++
			+		T	+		1	+	3000			H	H

PAMSONS
ESTIMATE WORKSHEET

M.T.O. BY					17	88			SHEET	0,	1
JOB NO.:	10		TYPE	TYPE OF ESTIMATE	LRE FO	EASIGILITY.	-		CHECKED BY	and	,
UNIT/AREA	40 WATER SUPPLY	OUAN.	7IN	COST OR M/HRS	MATERIAL	SUBC	SUBCONTRACT		LABOR	T07/ L	
CAPACITY ACCNT	PAKEGTE		MATL	M/H LABS		M/HR8	DOLLARS	MATHERS	DOLLARS		ž
	PLOE SLEEDERS (C')	7300	8	26			16300			\parallel	11
	PLOE UNCUORS (CIP)	35	D)	2076			1/180			H	11
11	PLOE SLEEPERS (3')	820	EA	30			16000			H	11
											
								Ш		#	+
4100	TOTAL HAER 40	7.39	≫ -				2/3000		72	21.5	8 8
200	CES 2000 0 (4/81)		H							2.70	I

ESTIMATE WORKSHEET

			3	3	8			SHEET	10
UNITABLE 40 11) PEC SUPPLY	-	COST OR M/HRS			SUBCONTE	BI INCOMPRINGE		CHECKED BY	
DESCRIPTION LAILEDA SULOWING STUDY.	TITY	PER UNI	T	EXPENSE	200	200	,	unda.	TOT/L DOLL/ RE
SADO PLON VALVES, FITTINGS ALG	++	MATL M/H LABS	LABS		M/HR8	BOLLARS	M/HMS	DOLLARS	
SEE DETHILS	306/00			C31720			277780		
FRT 3%	426		\parallel	23.80					-
PROV. 10 50%							76.84		\parallel
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PARSONS ESTIMATE WORKSHEET

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DESCRIPTION	OUAN.	S TIN	COST OR M/HRS	HRS	MATERIAL	SUBCONTRACT	Ct	5	LABOR	TOTAL
CAPACITY	+	MATL	M/H	LAB\$		M/HRS DOLLARS	H	M/HRS	DOLLARS	Service of the servic
Pipis - 1/a										
Who Piets										
		H								
Rolling Marnin Torrais:		+								
String Intell & weld out		+								
Dyelia	,	-						1		
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"15 0.321,"WALL 9"	3)	3							*	
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	CERM	01 3	۲,							
- 1										
Plains Toward :							+			
J. 6 0. R. 2. 1. 1. 1. 1.		+,					+		-	
	1.	13	11.							
		-					+	1	-	
115 0.316 Jal. 8	95.30	41 -14	يخ						+	+
11/10 Les F. Hair 94 A. (102.										
10 2)	(47	7 days	70.00							
Relief Whos 10.4 A-1	12.6	DA 400	22							
Thus all talves 100 hay	_		20							
MTO Allower Shats Row's Rough	7	-						-		-
(10% mall)	7	-47 4. Share	Zano							
Total 8.3.4 Aug	99	KA		1	02/88/20		7	22171	-	1

PARSONS

DESCRIPTION CAPACITY ACCUT ELECTRICAL ACCUT AC		200				5	DATE	10/22/88	6			SHEEL	1		_
TY ELECTRIC	CLIENT: CHILE		-	TYPE OF ESTIMATE	ESTIN	ATE						CHECKED BY			_
ELECT ZSKYA NE	WATER SHOPLY	OUAN.	TIN	COST OR M/HRS	HWH H		MATERIAL		UBCO	SUBCONTRACT		LABOR		TOTAL	_
ELECT 25KYA 1E				MATL	M/H	LABS	EAFENS	M/HRS	\vdash	DOLLARS	M/HR8	DOLLARS	100	ARS	
25KYR XEMER	76														- 44
2	Cat Krivanov	-	83	1	+	1	V	8	1	+	1			+	8.5
can mire our	OWETORDE TYPE		1					3	H	H	9				, ,
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TOTAL						3	.5	000	\dagger		9	Š		0	
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PAMECINE ESTIMATE WORKSHEET

JOB NO.:					ā	DATE //	3				٠			
NIT/AF	6905-1		TYPE	TYPE OF ESTIMATE	1	Pos A	FERSIBILITY	11/2			CHECK		The second	1
EBCHIP	" CHILEDKI SULDNUR	OUAN.	TIN	COST OR M/HRS PER UNIT			ans.	BUBCONTRACT	15	1	LABOR		2	TOTAL
ACCITY		+		MATL : M/H LABS	ABS		M/HPB	DOLLAM	8	MATHER	DOLLARS	ARS) I
	YUMMAK 9		+					1			1	1	+	1
1500	PUMPS 4 DRIVERS		H			146 000	0					F	t	+
3700	LAUNDERS		-		1			9	000					
3300	IHICKNERY & THICKENING ARCHANISMS					300		011	0000					
П	1 1		\parallel		\forall									
	7 D D OF		-		1	446,000	0	911	980				H	H
	FAEICHT	8%	\parallel		\dagger	36 000							+	
T	TOTA MATOR CONIDUCAT	1	1	1	1			1	1	-	-	1		
			-	1	+	482 000			ê		1	1	1	+
	FACTORED TOTAL		-		+	-			1	A.A.	-		+	1:
	CONC. LECORRY DUCHORS				1	-				T	1		7	
T	MOENAUVES FIRMOS							30	13	ľ		-	\dagger	+
	OTHER WINE (THILINGS DAM)							12.7	3					+
T	VITE 1-160							4/60	000					-
T	(202)		1	1	1			77	0				7	180
	Torse Courses nor horse				+	1					H		H	H
	LAN JEGEN		-		+	+		1	1		+	1	2	8
	MASOR KOULD 482K		-		t			t	1		+	1	+	+
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PAMSONS
ESTIMATE WORKSHEET

M.T.O. BY	LUCEDBI	AN				1							
JOB NO.	29a5-1		٤	TYPE OF ESTIMATE	MATE	LRE FO	603/B/LLT	LITZ			CHECKED BY) A8	1 W
UNIT/AREA DESCRIPTION	THION PAINEDLE SILL ONLY STUDY	OUAN.	Z IN	COST OR M/HRS	turni.	MATERIAL	SUBC	SUBCONTRACT		2	LABOR		TOTAL
CAPACITY	, , , , , , , , , , , , , , , , , , ,	+	MATL	TL M/H LAB\$	_		M/HR8	DOLLARS	1	M/HR8	DOLLARS	+	OL LA RS
3700	MOBILE AINING EQUIPMENT		+		T				+			+	1
	FEL 992 G	-	EA			688 000					F	-	t
	_	9	346	000	90	2 076 000							
	6-0 7	-	-			346 000							
	D02ER, n-8	1	+		1	234 000							
	2		+	1	1	278 000						300.00	
	TRUC	-	+	1	1	\$3 000							
	LUBE FUEL TRUCK	1	+		1	64 000							
	116		+		1			1					
	FORK	1	+		1	000 50							
	- 1	-	+		1	40 000			1				
	MAN BUS	-	+		1	25 000		-	+	1	1	+	
	AMBULANCE		1		1	-							
	11P w /MO	3	000	00	1	48 000							
	TATION		1		1								
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FAMETE WORKSHEET

		TYPE OF	TYPE OF ESTIMATE	Perfe	EBSIBILIT	The state of		CHECKED BY	The of
CHILLIAN SULDANE STIDE	OUAN.	COST OF	COST OR M/HRS	MATERIAL	SUBCC	SUBCONTRACT]	LABOR	_
	+	MATL M	M/H LABS	EXTENSE	M/HR8	DOLLARS	M/HPI8	DOLLARS	DOLL/ RE
SUMMARY									
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- 1				1 126 000					
REDUCTION EQUIPMENT				1 716 000					
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MAJOR EQUIPMENT				t.		ı			
MINING EQUIPMENT	1		1	195 bog					
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PAMSONS ESTIMATE WORKSHEET

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M.T.O. BY PRICED BY				DATE ///	88			SHEET		
1-10/0		TYPE	TYPE OF ESTIMATE	HEE F.	EASIBILITY	יאנה		CHECKED BY	nucl	
DESCRIPTION CHILEAN SULDAUR STUDY	OUAN.		COST OR M/HRS PER UNIT	1	SUBC	SUBCONTRACT		LABOR	1	V .
ACONT AULINES	+	MATL	M/H LABS		M/HR8	DOLLARS	M/HR8	DOLLARS	BOLLY	ي ي
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TOTAL		45	50/10/11	Ų.					180	18
TERTINAN (SN) L'AUCHRE 22 MX 17 MX 40M	25000		11:			1670a				
FONS (10) DENOXIVED 110%	30 60		200			(Com)				
TOTAL		7/1/2	180 / 4/80	tce					7	8
4900 Tayal NOEA 10	16/100 G	93.71	,			20,000		3	Joseph Company	
CER 2000 0 (4/6)					1	-				T

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PAMSONS
ESTIMATE WORKSHEET

M.T.O. BY					۵	DATE ///	88			SHEET	-	1
JOB NO.:	6905-1 CLIENT: 1		TYP	TYPE OF ESTIMATE	MATE	PRE F.	ERSIBILITY	. KIM		CHECKED BY.	apre	7
NIT/A	FOUT SUI CHUP	OUAN.	7 IN	COST OR M/HRS		4	SUBCK	SUBCONTRACT		LABOR	101/1	1 2!
CAPACITY	, , ,	+	MATL	L M/H LABS		EXPENSE	M/HRS	DOLLARS	M/HM8	DOLLARS		¥
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PAHSONS ESTIMATE WORKSHEET

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JOB MO:	27/45-		TYP	TYPE OF ESTIMATE	MATE	1987	FEBSIBILLITY	3778	7			CHECKED BY	'an	5
DESCRIPTION	PTION CHILEGAL SULCAUR STUDY.	OUAN.	S S	COST OR M/HRS PER UNIT	-	MATERIAL		MODEL	BUBCONTRACT		7	LABOR	TO	T077 L
CAPACITY	<u> </u>	-	MATL	M/H	LABS	CATCHOL	BA / HORES	\vdash	DOLLARS	H	DATE STATES	DOLLARS	8	ž O
ACCINT	SUMMARY													
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2100	REDUCTION EAVIPMENT					000 000	8	-	-					1
2600	BINS & CHUTES							-	9	000				1
2700	CLASSIFICATION & SCREENING EQUIP					120 00	000				000000000000000000000000000000000000000			_
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ON BO	5925		TYPE	TYPE OF ESTIMATE	POF.	FEASIBILITY	17		CHECKED BY	.1	11
UNIT/AREA DESCRIPTIO	ON CHILEGIN SULCHUR	OUAN.		COST OR MIHRS	MATERIA	SUBCO	SUBCONTRACT		LABOR	T0701	1 ~
ACCNT 4900	Burniska		MATT	M/H LAB\$		M/HR8	DOLLARS	M/HRS	DOLLARS		¥ -
	CALL MILL BUILDING 26 mx 15 mx 15 m (USE SECONDARY CRUSH-BRED 10)	30Mac		95/			346000				
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ab to	Tayor Hoes 15	30/100		D /							
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(090.5-1	CLIENT: OMILE		1	2020	-	DATE	138/	8.8				0F /	1
18 681	GRINDING	QUAN.	TIV	COST OR M/HRS	COST OR M/HRS	MATERIAL		SUBCONTRACT	-	CHEC	KED BY	TOTAL	
ACCINT ELECTRICAL				MATL M/	M/H LAB\$		M/HR8	DOLLARS		M/HPS DO	DOLLARS	DOLLARS	
SOOKING Y PRICE LILLED	4.647 /490V		3			13000				00/			
Tornt					*2	1300				100	8	(38	3 8
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ESTIMATE WORKSHEET

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JOB NO.:	CLIENT:		TYP	TYPE OF ESTIMATE			*			CHECKED BY	101
UNIT/AREA DESCRIPTION	45 TRILING & ROCLAIM WATE	OUAN.	NIN S	COST OR M/HRS		MATERIAL	SUBC	SUBCONTRACT		LABOR	TOTAL
CAPACITY		-	O MATL		M/H LAB\$	EXPENSE	M/HRS	DOLLARS	M/HR8	DOLLARS	DOLLARS
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FAMSONS
ESTIMATE WORKSHEET

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TRUENCE CAVIL Albak A WITH AND WATH WITH LAND WITH DOLLAND CRIPTION CHILLIANS SULCAURE STUDY		COST OR M/HRS PER UNIT	MATERIAL	SUBCONTRACT	LABOR	TOTAL	
Anter Clivic Work Thirting Dean. South Rock Compactor Fire Price of 1000 of	ACITY	+	M/H		\rightarrow	Н	DOLL R
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Finder Dress. / 65 Tayou dress 45.	V. Perstonegro		3		7		
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PAMSONS
ESTIMATE WORKSHEET

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JOB NO.:	: 6905-1 CLIENT: MECA		TYP	TYPE OF ESTIMATE		Per Fi	FEASIBILITY.	LITY.		CHECKED BY	and
UNIT/AREA DESCRIPTIO	" TAILEDA SUI DAUR	OUAN.	7 IN	COST OR M/HRS		<	SUBC	SUBCONTRACT		LABOR	T07/L
CAPACITY	0.00	+	MATL	L M/H LABS		CAFENSE	M/HR8	DOLLARS	M/HM8	DOLLARS	
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PARSONS

JOB NO.:	7 19070111	Carl I				0	DATE	1/	001						
	2905-1 CLIENT: CHILE			TYPE	TYPE OF ESTIMATE	MATE	1	and sold	100			CHECK	CHECKED BY	D. Wall	K
UNIT/AREA DESCRIPTION	ON AMER WE TRILING & RELIGION	OUAN.	TIN	COST	COST OR M/HRS		MATERIAL		SUBCONTRACT	TRACT		LABOR		TOTAL	با
CAPACITY				MATL	M/H LABS	_	EXPENSE	M/HRS	\mathbf{H}	DOLLARS	M/HRS	DOLLARS	ARS	ספרר	ARS
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ESTIMATE WORKSHEET

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DOB NO.: 6905-1 CLIENT: POWINTAREA SQ POWING SUICAUME SUI	Sulphur Sylloy Sulphur Sylloy NKS	OUAN. TITY	OF EST		N	FEASIBILITY	UN.		CHECKED BY	COME	
	_		COST OR M.	_							,
	AKS			-		SUBCO	SUBCONTRACT	-	LABOR	T07/L	1
44444444444444	BANES		MATL M/H	LABS		M/HM8	DOLLANS	MA/HPRS	DOLLARS	-	2
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Sunolytes Sure Hork Fire Hork Tryac Caus	Torac									3.70	900
TOTAL CAN				+						1	
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PAMSONS ESTIMATE WORKSHEET

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M.T.O. BY					DATE ///	88				SHEET	
JOB NO.:	1-3085			TYPE OF ESTIMATE	Per	FEASIBILITY	1117	,		CHECKED BY	0
UNIT/AREA DESCRIPTIO	CHILFON SULCHUR	OUAN-	TIN	COST OR M/HRS	MATERIA		BUBCONTRACT	+	2	LABOR	TOTFL
ACCNT 4900	Burrondes			MATL M/H LAB\$		M/HR8	DOLLARS	AR8	M/HHRS	DOLLARS	Merca
	POWER GEN PLANT	10,000	o.	34			r.				
	HOD JUSSUL SIGNAGO M.640	13000	8	8:			11	8			
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ESCR!	DESCRIPTION CHILEDA SULDAUR STUDY	OUAN.	5 TIN	COST OR M/HRS			BUBCONTRACT	•	LABOR	T01/ L
ACCINT ACCINT	SUTE PREP	+ +	MATL	L M/H LABS		M/HR8	DOLLARS	M/HRS	DOLLARS	
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FARSONS ESTIMATE WORKSHEET

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TITY SECTOR WHIS SUBCONTRACT LABOR TITY SECTION WHIS BOLLARS WHEN DOLLARS	JOB NO.: 69	105-1 CLIENT: CHILE			LYPE 0	F ESTIMA	TE		1			CHECKED 8	1	
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# (18 (13 00 1500 6, 2000) # (18 (13 00 1500 6, 2000) # (2000) # (2000) # (2000)	PACITY	ELECTRICAL				M/H LA			M/HRS	DOLLAR		H	1	ARS
20005 20002 20	DIES 327K	EL ENGINE GENERATOR		CB	7800	2500	19	0000			10,00			
\$5500 \$5000 \$5000	3/10	KW GOORPM GILKY												+
1, 15 LS LS (100000)	Stala	REGESS AND DEOTECTIVE				+								+
2005 - 57 57 LJ 0005	7415	PLLEY - MARPLESS BLACKS	DALE							H				+
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2005 FT 45 45 (100000)	5.019	540 + 3 - 1/475, 180/50			\dagger									
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5000 FT 45 45 REGER	(1880)	NG BETWEEN SUBRE & BEAR	1	57	5	5,	9				1000			
2000 FT & 2 L S A	13.2	KV TRANSMISSION LINE		-	-			1			8			
2000S	SA	LOMBTERS - TO SUBSTAN	7	\dagger	\dagger	+								
2000 FT 45 45	Day	O KIN BUCKD GO HISTORY	¥											
	13.2	KV DISTRIBUTION LINE		1		4				1 4				
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1							680	one		RADA	11000	2		

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FSTIMATE WORKSHEET

M.T.O. BY	The second secon				•	11/ 3100								
JOB NO.:	6905-1 CLIENT: MECA		TYPE	TYPE OF ESTIMATE	MATE	PRE	FERSIBILITY	111			CHECKED BY	KED BY	MAN	1
UNIT/AREA DESCRIPTION	LANGON SUI ONLINE	OUAN.	NIT S	COST OR M/HHS PER UNIT	HRS	MATERIAL		BUBCONTRACT	t		LABOR		P	TOTAL
CAPACITY		+	MATT	M/H LABS	NB 8	CALENDE	M/HPS	DOLLARS	ARS	BA/HFRB	DOLLARS	ARE	00	ا چ
ACCNT	SUMMARY		+											
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PACHSONS
ESTIMATE WORKSHEET

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M.T.O. BY						DATE ///	88			SHEET	30	F
JOB NO.:	D: 6905-1 CLIENT: MECA		7	TYPE OF ESTIMATE	TIMATE	PRE F.	CERSIBILITY	- KUM		CHECKED BY	10	L
UNIT/AREA DESCRIPTIO	< 1 ≥	OUAN.	TIN	COST OR M/HRS PER UNIT	I/HRS	MATERIAL	SUBC	SUBCONTRACT		LABOR	1017.1	
CAPACITY	T.			MATT. M/H	M/H LABS	TO LEASE	M/HR8	DOLLARS	M/HPRS	DOLLARS	1	£
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FARSONS
ESTIMATE WORKSHEET

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SHEET	CHECKED BY	LABOR	DOLLARS														-		1	1	70,	7						
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	GASIBILITY.	SUBCONTRACT	DOLLARS		166.00	#	8600	2000	1600	#	1	78.000	THE W			20,000		1 4		Sales Sales	10.000	2000		63,4000		000/79		60/00
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ò	TYPE OF ESTIMATE A	COST OR M/HRB	M/H LABS		34			Man	50/		(oac)		320		100	3.00.1	200							2 07				
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	6905-1 CLIENT: MECA	NO AUTORY FACILITIES	The same of the sa	Burowes (couto)	Staff Quel	(1) (f. 1) Correct Correct	CONCRETE TOWN :3 X1:	DOD PLUMBING	INTRESE PRETITIONS	(00 3800 W)	FULNITURE	Î	Mexs & Veresona	en x is m)	6/01/Chr/2-4041001 202	FON (10) 6x6x 2/27/0 110%	Car der B 290x,5 x 2,570 1000	7	FRON SERVICE COMPO	FURTITURE	Social Finishes	Cornel			(1.16 Med Dourse	CONCRETE	mod Found (stor Found	Torac
M.T.O. BY	HOB NO.	UNIT/AREA DESCRIPTION	CAPACITY	4400																ļ				1	*			

PAHSONS

32,000 of 3 1000 TOT/ L DOLL/ RE SHEET 3 CHECKED BY DOLLARS LABOR M/HR8 24 pm 1/000 Moss M/HRS DOLLARS BUBCONTRACT PRE FEASIBILITY MATERIAL **ESTIMATE WORKSHEET** TYPE OF ESTIMATE MATL M/H LABS COST OR M/HRS PER UNIT 26 1/10 200 202 200 \$5090 SF 72.7 B 5 TINO 35090 3/100 29 16600 TITY GROW: LOOK. 67 X LAI P. 198% DESCRIPTION CHILEDAN SULDAUR STUDY CATTON (COMPLETE PRICED BY Faits (4) externs CLIENT: MECA BunDINGS (CONTO TOTAL MESO 60 OFC FURNITURE OF GWC-DEG UNIT/AREA 60 CAPACITY JOB NO.: 4900 M.T.O. BY ACCNT

CES-2000 0 (4/81)